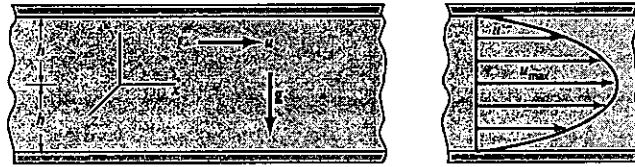


**Problem 1. (20%)**

Consider an incompressible Newtonian fluid flowing through a gap (height =  $2h$ ) between two parallel plates. The fully developed laminar flow velocity profile  $u(y)$  can be determined by solving the x-component Navier-Stokes equation, where  $u$ ,  $v$ , and  $w$  are fluid velocity components along  $x$ ,  $y$ , and  $z$  direction, respectively.



$$\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = -\frac{\partial p}{\partial x} + \rho g_x + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

- (a) Explain that the above equation is a result of momentum balance. (5%)
- (b) Prove the velocity profile below. (5%)

$$u = \frac{1}{2\mu} \left( \frac{\partial p}{\partial x} \right) (y^2 - h^2)$$

- (c) Show that the volume rate of flow is proportional to  $h^3$ . (5%)
- (d) Use a schematic to illustrate how the velocity profile  $u(y)$  changes for turbulent flow. (5%)

**Problem 2. (20%)**

- (a) Explain fluid friction loss from the Bernoulli equation. (5%)
- (b) Write down the physical significance and unit of the Fanning friction factor as defined below. (5%)

$$f \equiv \frac{\tau_w}{\rho \bar{V}^2 / 2}$$

- (c) Justify the following equation for a laminar pipe flow, where  $\Delta p_s$  is the pressure drop due to skin friction,  $\tau_w$  is the shear stress at the wall of the pipe,  $D$  is diameter of the pipe, and  $L$  is the length of the pipe. (5%)

$$\Delta p_s = 4(\tau_w/D) \cdot L$$

- (d) Use a schematic to compare how  $f$  varies with  $Re$  for laminar flow and turbulent flow, respectively. (5%)

**Problem 3. (20%)**

Consider that a thick beef steak is being baked on a hot plate with a surface temperature  $T_s$ . Before baking, the raw beef steak is placed at room temperature ( $T_0$ ) for a sufficient long while, so the temperature distribution is uniform throughout the raw steak initially. Here we only model the first-stage of steak baking (*i.e.*, without flip-side), and the steak thickness is sufficiently large so that the following semi-infinite transient heat conduction model can be applied.

$$\frac{T - T_0}{T_s - T_0} = \text{erfc} \left( \frac{x}{\sqrt{4\alpha t}} \right)$$

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- (a) Write down the physical meaning and SI unit of  $\alpha$  in the above equation. (5%)
- (b) Give the partial differential equation and related initial and boundary conditions for obtaining the above temperature profile model. (5%)
- (c) Use a schematic to compare the temperature profiles  $T(x)$  at small, middle, and large time  $t$ . (5%)
- (d) Determine the heat flux required as a function of time  $q(t)$  to bake the steak. (5%)

**Problem 4. (20%)**

- (a) Derive the Fick's second law from the Fick's first law. (7%)
- (b) Below is the Einstein diffusion equation.

$$c(x, t) = \frac{c_0}{\sqrt{4\pi Dt}} \exp\left(\frac{-x^2}{4Dt}\right)$$

Show that the mean squared displacement of a molecule for one-dimensional diffusion is  $2Dt$ . The following exponential integrals are useful. (7%)

$$\int_{-\infty}^{\infty} e^{-ax^2} dx = \sqrt{\frac{\pi}{a}} \quad \int_{-\infty}^{\infty} x^2 e^{-ax^2} dx = \frac{1}{2a} \sqrt{\frac{\pi}{a}}$$

- (c) For sucrose in water at 25 °C,  $D = 5 \times 10^{-6} \text{ cm}^2 \cdot \text{s}^{-1}$ . Assume that in a region of an unstirred aqueous solution of sucrose the molar concentration gradient is  $-0.2 \text{ M} \cdot \text{cm}^{-1}$ . The amount of sucrose molecules passing through a  $10 \text{ cm}^2$  window in 10 min is  $X \mu\text{mol}$ .  $X = ?$  (6%)

**Problem 5. (20%)**

Serum creatinine (denoted as A), a detectable byproduct of muscle metabolism, is viewed as a biomarker of kidney health because it is removed from the blood mainly by the kidneys (the so-called "creatinine clearance"). It is known that creatinine has a constant half-life ( $t_{1/2}$ , hr) while removed in the kidneys (*i.e.*, obeying first-order kinetics). Now, an organ chip as well as a microfluidic PFR (plug-flow reactor) made of 3D human kidney cell culture coated on the microfluidic channel walls is fabricated for creatinine metabolism study. The microfluidic PFR has a cross-section area of  $S \text{ (}\mu\text{m}^2\text{)}$  and a length of  $L \text{ (cm)}$ , and an artificial blood stream containing a creatinine concentration of  $C_{A0}$  is pumped into the kidney-PFR chip at a constant volumetric flow rate  $v_0 \text{ (}\mu\text{l/hr)}$  for the study.

- (a) Draw a schematic to illustrate the PFR-mimic microfluidic kidney chip for creatinine removal study. (5%)
- (b) Perform mass balance for a PFR reactor to relate the reactor volume to conversion  $X$  for a first-order chemical reaction. (5%)
- (c) Show that the length of the microfluidic PFR kidney ( $L$ ) can be modeled as follows. (5%)

$$L = -\left(\frac{t_{1/2}}{\ln 2}\right) \left(\frac{v_0}{S}\right) \ln(1 - X)$$

- (d) Comment what would be different if the microfluidic organ chip was modeled by a packed-bed reactor instead of a PFR. (5%)