

1. Match the following descriptions with the figures shown in Fig. 1. Fields are near the interface but on the opposite sides of the boundary. (12%)

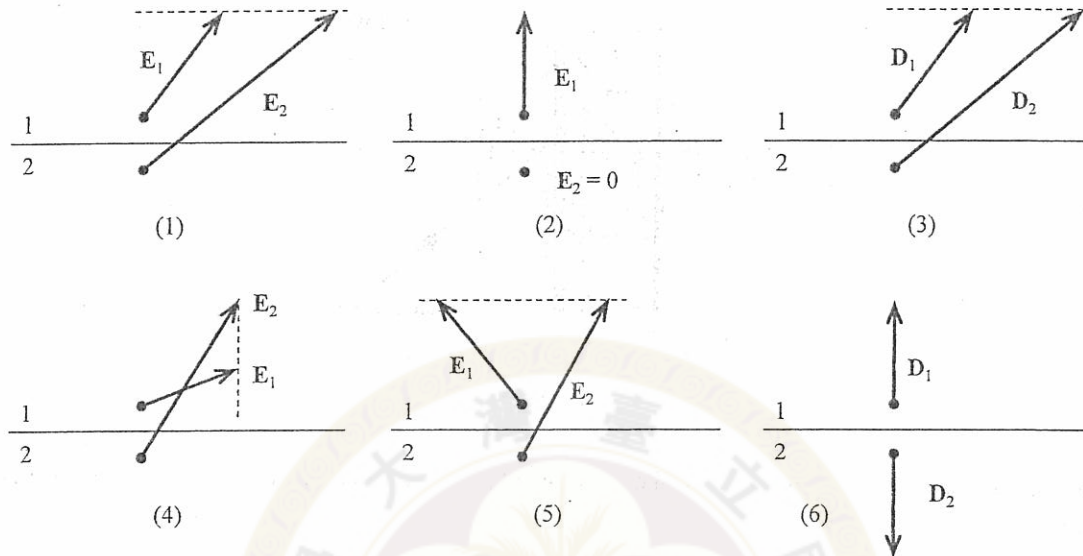


Fig. 1

- (a) medium 1 and medium 2 are dielectrics with  $\epsilon_1 > \epsilon_2$   
 (b) medium 1 and medium 2 are dielectrics with  $\epsilon_1 < \epsilon_2$   
 (c) impossible  
 (d) there is a positive surface charge on the boundary between two dielectrics  
 (e) medium 2 is a perfect conductor
2. Find the static potential distribution  $\phi$  between two infinite parallel plates. One plate is located at  $x = 0$  with  $\phi = 0$  V, and the other is located at  $x = 1$  with  $\phi = 1$  V. The space between the plates is filled with a medium having a constant permittivity  $\epsilon$  F/m and a varying electric charge density  $\rho(x) = -\epsilon(x+1)$  C/m<sup>3</sup>. (8%)
3. Skin depth  $\delta$  has been defined as  $k_{c,im}\delta = -1$  for highly conducting media, where  $k_{c,im}$  represents the imaginary part of the complex wavenumber in the medium. Following the same definition, please determine at 1 GHz the skin depth of (a) a perfect conductor, (b) a lossless medium, and (c) a slightly conducting medium with  $\sigma = 10^{-6}$  mho/m and  $\epsilon \approx 3.2\epsilon_0$ . [ $\epsilon_0 = 8.85 \times 10^{-12}$  F/m] (8%)
4. A uniform plane wave is incident upon a homogeneous dielectric slab backed by a perfect electric conducting plane. The dielectric slab has thickness  $L = \lambda$  (free-space wavelength), relative permittivity  $\epsilon_r = 8$ , and relative permeability  $\mu_r = 2$ . The surrounding medium is free space having  $\epsilon_r = \mu_r = 1$ . The electric field intensity of the incident wave can be represented by  $\vec{E}_{inc}(x, y, t) = \hat{z}E_0 e^{jk_0(x-L)\cos\theta - jk_0y\sin\theta} e^{j\omega t}$ , where  $E_0$  is a complex constant of the incident field,  $k_0$  is the free-space wavenumber, and  $\theta$  is the angle of incidence defined in Fig. 2. Please find the reflection coefficient  $\Gamma$  at the air-dielectric interface ( $x = L$ ) as a function of  $\theta$ . (10%)  
 [Hint: write down the total electric and magnetic fields within the  $0 < x < L$  and  $x > L$  regions, respectively, and then apply boundary conditions at  $x = L$ .]

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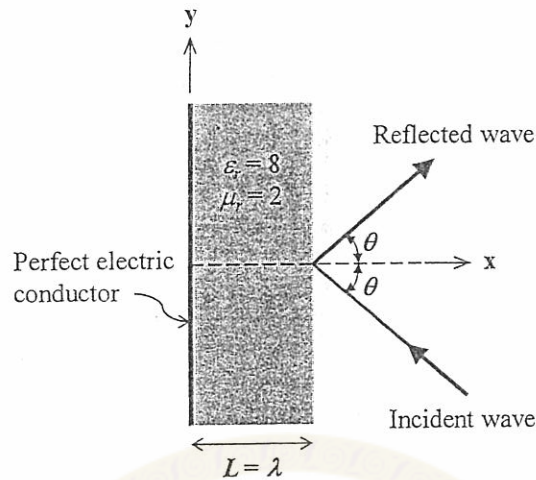


Fig. 2

5. The electric and magnetic field intensities radiated by an antenna located at the origin are given in spherical coordinates by

$$\vec{E} = E_0 e^{j\omega[t - (r/c)]} \left[ \hat{r} \cos \theta \left( \frac{2c}{j\omega r^2} - \frac{2c^2}{\omega^2 r^3} \right) + \hat{\theta} \sin \theta \left( \frac{1}{r} + \frac{c}{j\omega r^2} - \frac{c^2}{\omega^2 r^3} \right) \right] \text{ (V/m)}$$

$$\vec{H} = E_0 c \epsilon_0 e^{j\omega[t - (r/c)]} \hat{\phi} \sin \theta \left( \frac{1}{r} + \frac{c}{j\omega r^2} \right) \text{ (A/m)}$$

where  $c = 1/\sqrt{\epsilon_0 \mu_0}$

Find in the far zone: (a) the polarization of the wave radiated by the antenna, (b) the time-average Poynting vector, and (c) the time-average power radiated by the antenna by evaluating the surface integral of the instantaneous Poynting vector over a spherical surface of radius  $r$  centered at the antenna and enclosing the antenna. (12%)

6. A 100- $\Omega$  lossless transmission line is terminated with a load impedance  $Z_L = R_L + jX_L$ .
- (a) If the standing-wave ratio is 2 and  $R_L = 200 \Omega$ , Find  $X_L$ . (5%)
- (b) Where do the voltage maximum and voltage minimum which are the nearest to the load occur on the line for part (a)? (in terms of wavelength,  $\lambda$ ) (10%)
7. Fig. 3(a) shows a FET amplifier with input and output matching networks. In order to achieve the maximum gain, the reflection coefficients of the input and output matching networks should be  $\Gamma_{ms}$  and  $\Gamma_{ml}$ , respectively. Design the input and output matching network to achieve maximum gain of the FET amplifier.
- (a) If reflection coefficient  $\Gamma_{ms} = 0.4 + j0.2$ , calculate the corresponding normalized impedance  $z_{ms}$  (express in the format of  $r_{ms} + jx_{ms}$ ) and use the Smith chart shown in Fig. 3(b) to explain the impedance trace movement of the transmission line matching circuit shown in Fig. 3(c) for input matching network. (10%)
- (b) If reflection coefficient  $\Gamma_{ml} = 0.5 \angle 90^\circ$ , calculate the corresponding normalized impedance  $z_{ml}$  (express in the format of  $r_{ml} + jx_{ml}$ ) and use the Smith chart shown in Fig. 3(b) to explain the impedance trace movement of the transmission line matching circuit shown in Fig. 3(d) for input matching network. (10%)

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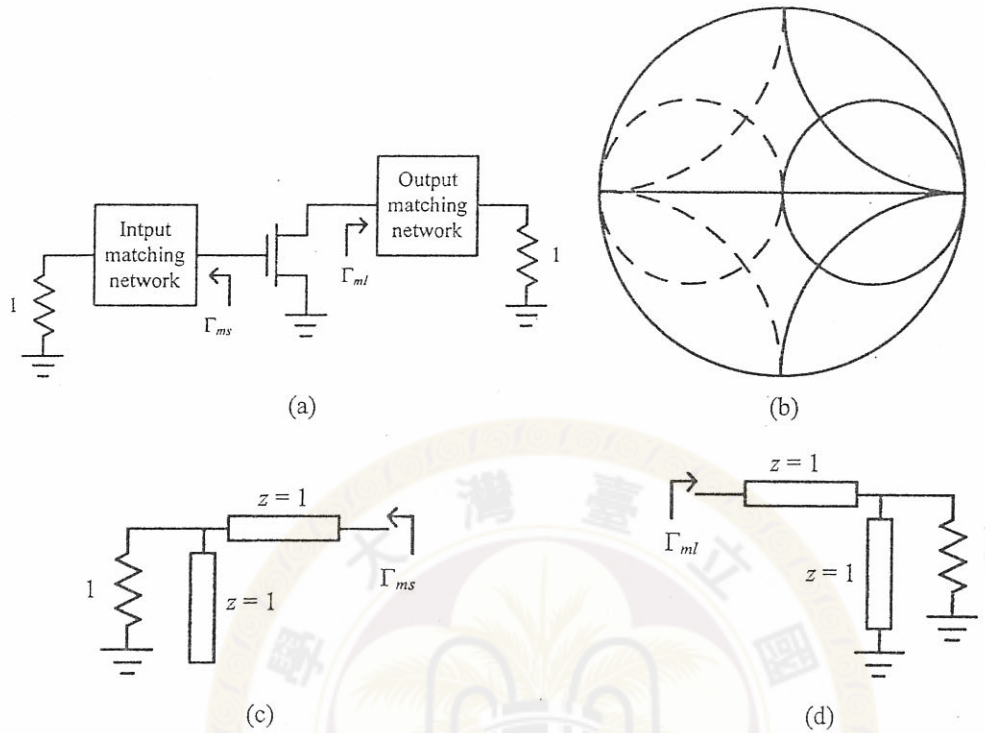


Fig. 3

8. A dielectric slab of thickness 2 cm and permittivity  $4\epsilon_0$  exists in an air-dielectric electric rectangular waveguide of dimensions  $a = 6$  cm and  $b = 3$  cm, as shown in Fig. 4. Find the lowest frequency for which the dielectric slab allows complete transmission for  $TE_{1,0}$  mode propagation in the waveguide. (15%)

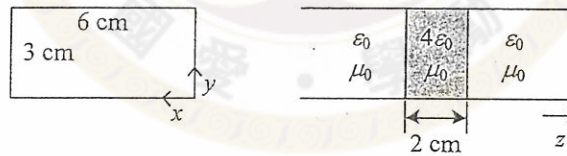


Fig. 4

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