

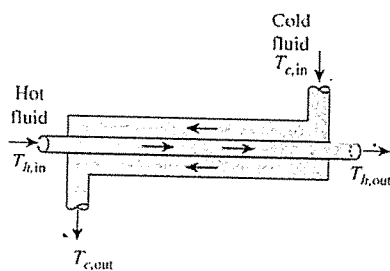
FIGURE 6.2 The Oswald viscometer.

1. a. To simplify the Navier–Stokes equations with appropriate boundary deriving the Hagen–Poiseuille equation for a vertical tube with inside diameter R and length L. (10%)
- b. Kinetic viscosity of a fluid can be measured using an Oswald viscometer by the following equation. How was the equation derived? t: elapsed time (10%)

$$\nu = \frac{\pi R^4 g}{8Vl} \cdot t$$

ν : Kinetic viscosity

$$\rho \left(\frac{\partial u_z}{\partial t} + u_r \frac{\partial u_z}{\partial r} + \frac{u_\theta}{r} \frac{\partial u_z}{\partial \theta} + u_z \frac{\partial u_z}{\partial z} \right) = -\frac{\partial P}{\partial z} + \rho g_z + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 u_z}{\partial \theta^2} + \frac{\partial^2 u_z}{\partial z^2} \right]$$

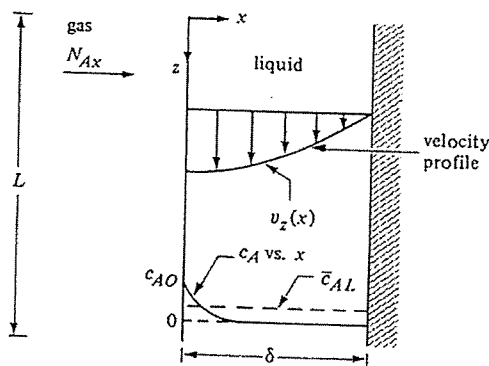


2. The log mean temperature difference method is frequently used in heat exchanger design.

- a. Using nomenclatures in fig. 2 to define the log mean temperature. (10%)
- b. Cold water ($c_p=4\text{kJ/Kg K}$) enters a counter-flow heat exchange at 5°C at a rate of 8 kg/s, and exits at 35°C , to chill processed

olive oil ($c_p=2\text{kJ/Kg K}$) at 50°C at a rate of 16 kg/s. If the overall heat transfer coefficient is 1000W/m^2 , determine the heat transfer area of the heat exchanger. (10%)

3. Gas absorption in a wetted-wall columns is schematically shown in fig. 3, The



solute A in the gas is absorbed at the interface and then diffuses a distance into the liquid so that it has not penetrated the whole distance $x = \delta$ at the wall. The operation is at steady state and the inlet concentration $c_A=0$. A simplified governing equation of diffusion in a laminar falling film is depicted as follow.

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$$v_{z=surface} \frac{\partial c_A}{\partial z} = D_{AB} \frac{\partial^2 c_A}{\partial x^2}$$

- a. To determine the local molar flux at the surface $x=0$ at point z . (10%)
 b. To determine the average molar flux over the entire length $z=0$ to $z=L$. (10%)

For your reference, temperature profile of transient heat conduction in a semi-infinite solid can be shown as,

$$\frac{T(x,t) - T_i}{T_\infty - T_i} = \text{erfc}\left(\frac{x}{2\sqrt{\alpha t}}\right) \quad \text{erfc}(x) = 1 - \text{erf}(x) \quad \frac{d}{dx} \text{erfc}(x) = \frac{2e^{-x^2}}{\sqrt{\pi}}$$

4. A filtration test was carried out, with a particular product slurry, on a laboratory filter press under a constant pressure (ΔP) of 340 kPa and volumes of filtrate were collected as follows: (20%)

Filtrate weight: V (g)	20	40	60	80
Time: t (min)	8	25	54.5	93

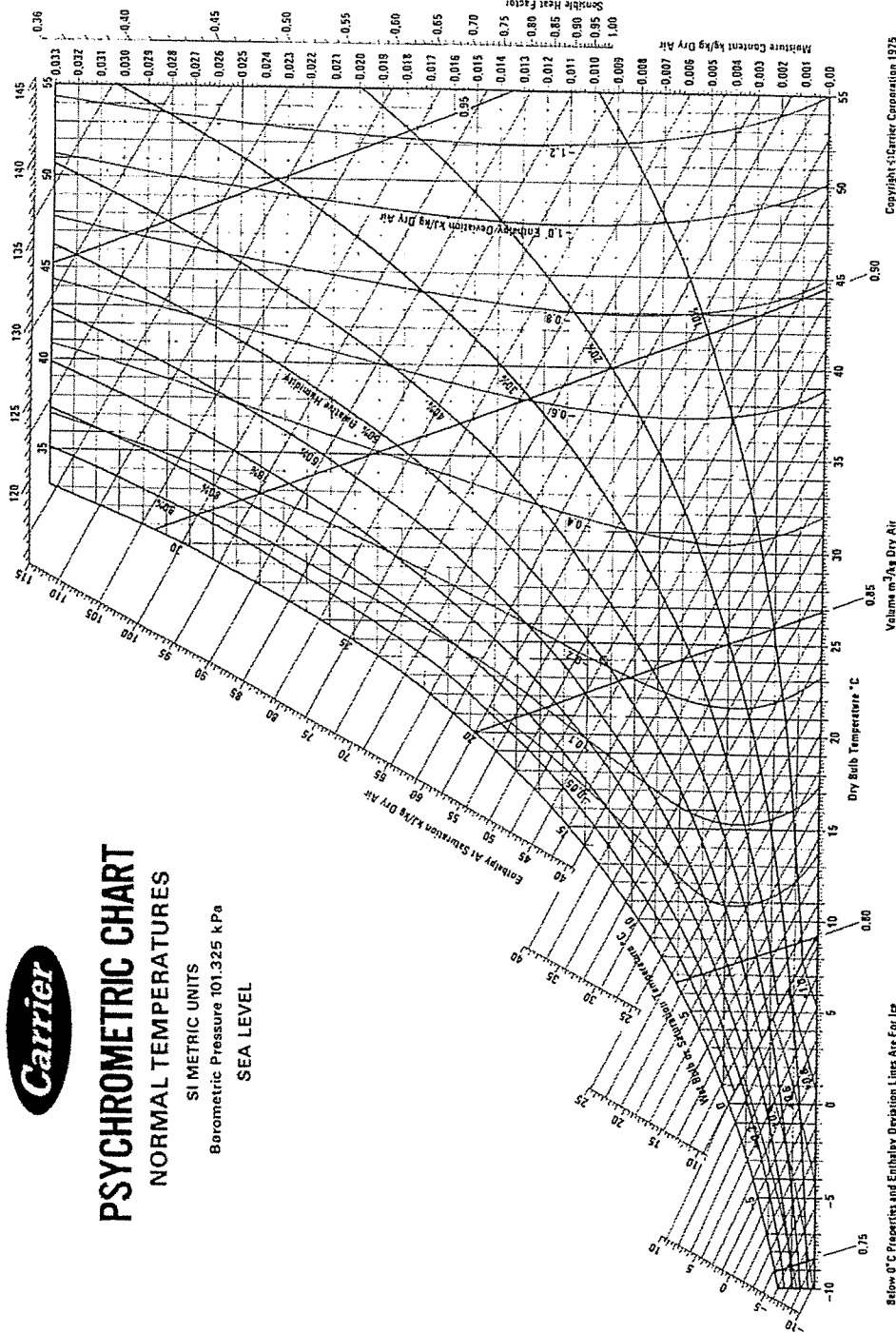
The area (A) of the laboratory filter was 0.186 m^2 . In a plant scale filter, it is desired to filter a slurry containing the same material, but at 50% greater concentration (w) than that used for the test, and under a pressure of 270 kPa. Estimate the quantity of filtrate that would pass through in 1 hour if the area of the filter is 9.3 m^2 .

$$t/(V/A) = (w/\Delta P)K(V/A) + K'/\Delta P$$

5. A counter flow dryer unit uses heated air to dry apple slices. The slices enter at a rate of 200 kg/h and a moisture content of $m_1 = 0.9(\text{WB})$. The "dried" slices have a moisture content of $M_2 = 0.10(\text{WB})$. The drying air enters at 50°C and exits at 25°C and 90% relative humidity.

- a. Find the water removed, (kg/h). (10%)
 b. Find the entering air flow rate, CMM(m^3/min) (10%)

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